

ENERGY PRINCIPLE

The term enthalpy = $h = \left(u + \frac{p}{\rho} \right)$

$$\dot{Q} - \dot{W}_s = \int_{A2} \left(\frac{p_2}{\rho} + u_2 + \frac{V_2^2}{2} + gz_2 \right) \rho V_2 dA_1 - \int_{A1} \left(\frac{p_1}{\rho} + u_1 + \frac{V_1^2}{2} + gz_1 \right) \rho V_1 dA_1$$

$$\dot{Q} - \dot{W}_s + \int_{A1} \left(\frac{p_1}{\rho} + gz_1 + u \right) \rho V_1 dA_1 + \int_{A1} \frac{\rho V_1^3}{2} dA_1 = \int_{A2} \left(\frac{p_2}{\rho} + gz_2 + u_2 \right) \rho V_2 dA_1 + \int_{A2} \frac{\rho V_2^3}{2} dA_2$$

It is common to express the term $\int \frac{\rho V^3}{2} dA = \alpha \left(\frac{\bar{V}^3}{2} \right) A$

Substituting for $\int \frac{\rho V^3}{2} dA = \alpha \left(\frac{\bar{V}^3}{2} \right) A$ in Eqn. above and dividing through by \dot{m}

$$\frac{1}{\dot{m}} (\dot{Q} - \dot{W}_s) + \left(\frac{p_1}{\rho} + gz_1 + u_1 + \alpha_1 \frac{\bar{V}_1^2}{2} \right) = \left(\frac{p_2}{\rho} + gz_2 + u_2 + \alpha_2 \frac{\bar{V}_2^2}{2} \right)$$

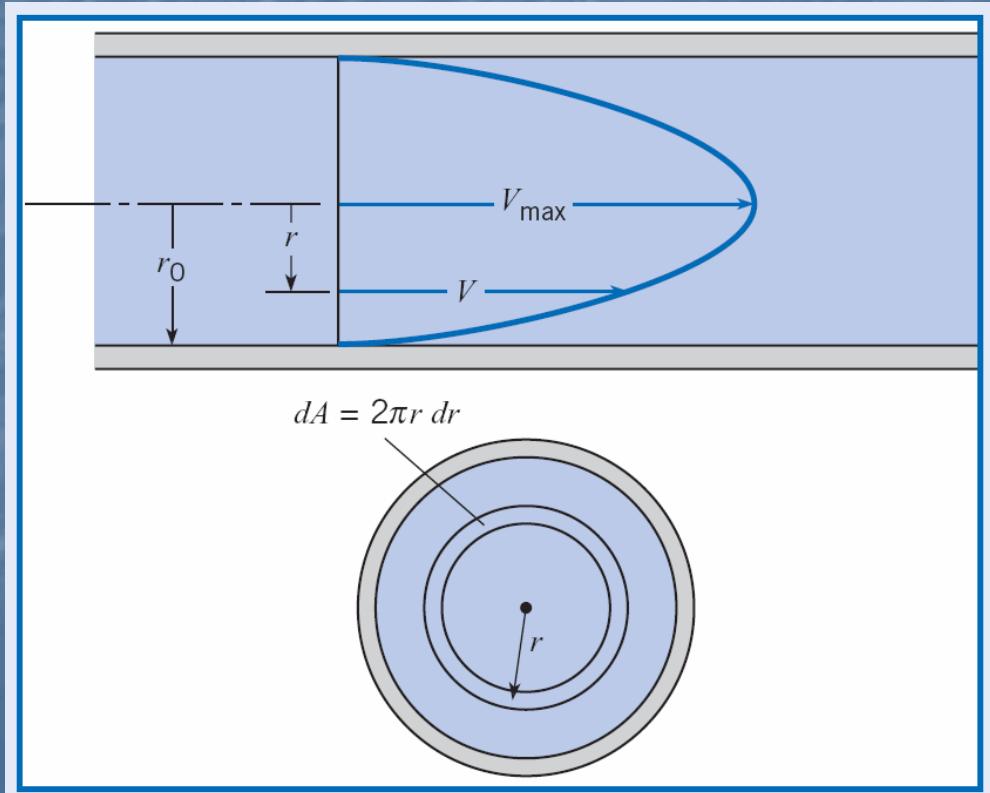
Example (7.2)

The velocity distribution for laminar flow in a pipe is given by the equation

$$V = V_{\max} \left[1 - \left(\frac{r}{r_0} \right)^2 \right]$$

Here r_0 is the radius of the pipe and r is the radial distance from the center. Determine \bar{V} in terms of V_{\max} and evaluate the kinetic-energy correction factor α .

Find: \bar{V} in terms of V_{\max} , α



Given: $V = V_{\max} \left[1 - \left(\frac{r}{r_0} \right)^2 \right]$

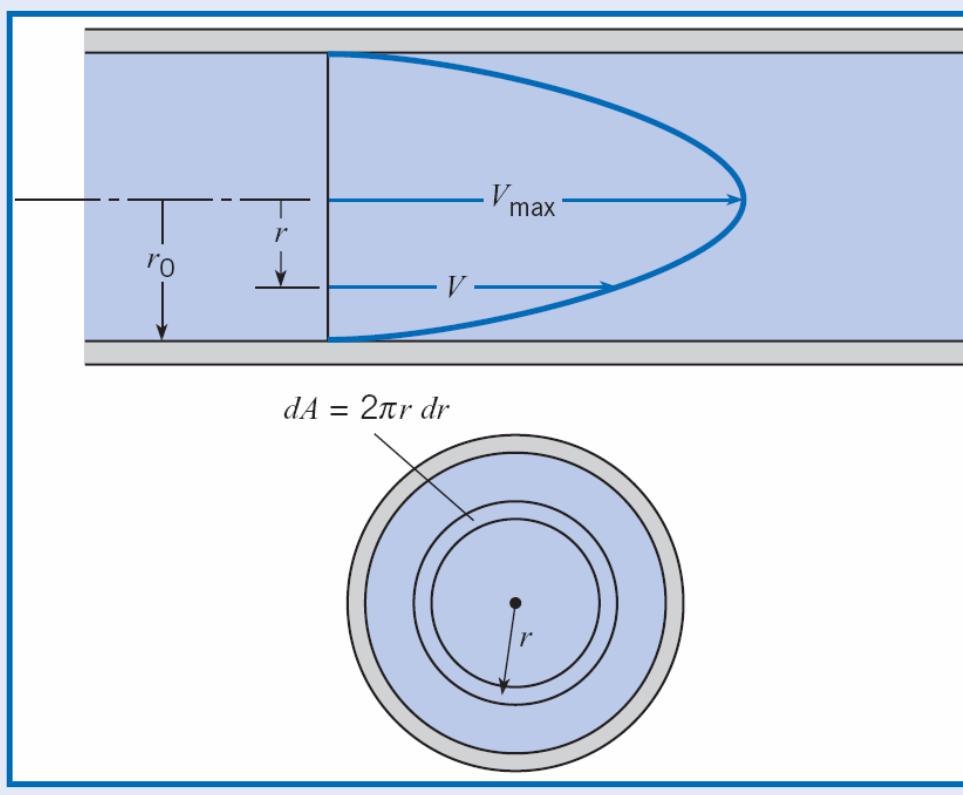
Solution

$$Q = A \bar{V} = \int_0^{r_0} V_{\max} \left[1 - \left(\frac{r}{r_0} \right)^2 \right] (2\pi r) dr$$

$$\bar{V} = \frac{-\pi r_0^2 V_{\max}}{A} \frac{(1 - r^2/r_0^2)^2}{2} \bigg|_0^{r_0} = \frac{1}{2} V_{\max}$$

$$\bar{V} = \frac{1}{2} V_{\max}$$

$$\alpha = \frac{1}{A} \int_A \left(\frac{V}{\bar{V}} \right)^3 dA = \left(\frac{1}{\pi r_0^2} \right) \int_0^{r_0} \left[\frac{V_{\max}^3 \left(1 - \left(\frac{r}{r_0} \right)^2 \right)^3}{\left(\frac{1}{2} V_{\max} \right)^3} \right] (2\pi r) dr = 2$$



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Pump – Turbine Combination

When a compressor and a turbine are connected together, the resultant shaft work \dot{W}_s is equal to

$$\dot{W}_s = \dot{W}_T - \dot{W}_P$$

Substituting for the above expression in Eqn. below

$$\frac{1}{\dot{m}}(\dot{Q} - \dot{W}_s) + \left(\frac{p_1}{\rho} + gz_1 + u_1 + \alpha_1 \frac{\bar{V}_1^2}{2} \right) = \left(\frac{p_2}{\rho} + gz_2 + u_2 + \alpha_2 \frac{\bar{V}_2^2}{2} \right)$$

and divide by (g), we have

$$\frac{\dot{Q}}{\dot{m}g} - \left(\frac{\dot{W}_T - \dot{W}_P}{g} \right) + \left(\frac{p_1}{\rho g} + z_1 + \frac{u_1}{g} + \alpha_1 \frac{\bar{V}_1^2}{2g} \right) = \left(\frac{p_2}{\rho g} + gz_2 + \frac{u_2}{g} + \alpha_2 \frac{\bar{V}_2^2}{2g} \right)$$

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Rearranging, we have

$$\left(\frac{\dot{W}_p}{\dot{m}g} \right) + \left(\frac{p_1}{\rho g} + z_1 + \alpha_1 \frac{\bar{V}_1^2}{2g} \right) = \left(\frac{\dot{W}_T}{\dot{m}g} \right) + \left(\frac{p_2}{\rho g} + gz_2 + \alpha_2 \frac{\bar{V}_2^2}{2g} \right) + \left(\frac{u_2 - u_1}{g} \right) - \left(\frac{\dot{Q}}{\dot{m}g} \right)$$

$$\left(h_P + \frac{p_1}{\rho g} + z_1 + \alpha_1 \frac{\bar{V}_1^2}{2g} \right)_{\text{Mech. part}} = \left(h_T + \frac{p_2}{\rho g} + gz_2 + \alpha_2 \frac{\bar{V}_2^2}{2g} \right)_{\text{Mech. part}} + \left(\frac{u_2 - u_1}{g} - \frac{\dot{Q}}{\dot{m}g} \right)_{\text{thermal part}}$$

$$h_P = \frac{\dot{W}_C}{\dot{m}g} = \text{Pump Head}$$

$$h_T = \frac{\dot{W}_T}{\dot{m}g} = \text{Turbine Head}$$

$$\text{The Head Loss} = h_{\text{Loss}} = \left(\frac{1}{g} \right) \left(u_2 - u_1 - \frac{\dot{Q}}{\dot{m}} \right)$$

$$\left(h_P + \frac{p_1}{\rho g} + z_1 + \alpha_1 \frac{\bar{V}_1^2}{2g} \right)_{\text{Mech. part}} = \left(h_T + \frac{p_2}{\rho g} + gz_2 + \alpha_2 \frac{\bar{V}_2^2}{2g} \right)_{\text{Mech. part}} + h_{\text{Loss}}$$

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$$\text{Pump Head} = h_C = \frac{\dot{W}_C}{\dot{m}g}$$

$$\dot{W}_C = \dot{m}gh_C = \gamma Qh_C$$

$$\dot{W}_T = \dot{m}gh_T = \gamma Qh_T$$

$$\text{Pump Efficiency} = \eta_P = \frac{(\dot{W}_P)}{(\dot{W}_P)_{actual}}$$

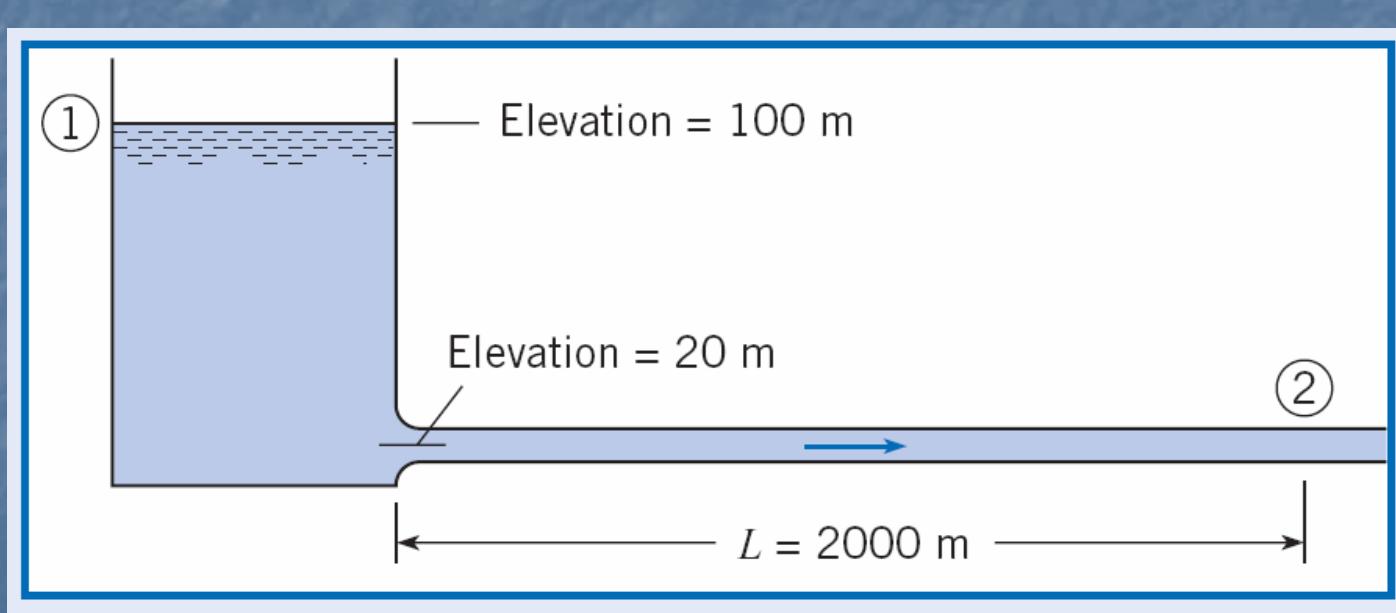
$$\text{Turbine Efficiency} = \eta_T = \frac{(\dot{W}_T)_{actual}}{(\dot{W}_T)}$$

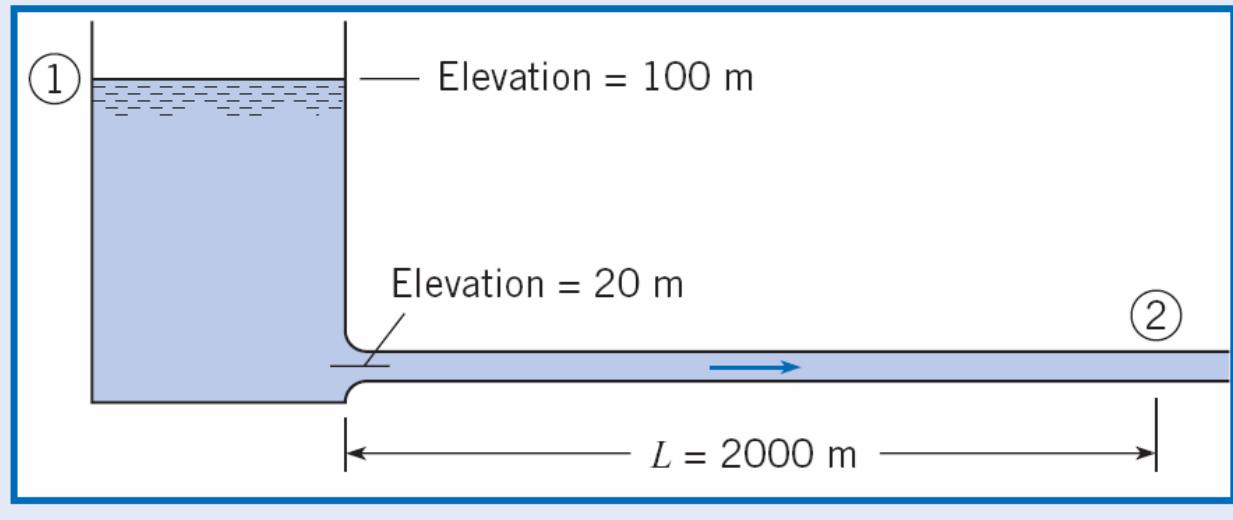
Example (7.3)

A horizontal pipe carries cooling water for a thermal power plant from a reservoir as shown. The head loss in the pipe is given as

$$\frac{0.02(L/D)V^2}{2g}$$

where L is the length of the pipe from the reservoir to the point in question, V is the mean velocity in the pipe, and D is the diameter of the pipe. If the pipe diameter is 20 cm and the rate of flow is $0.06 \text{ m}^3/\text{s}$, what is the pressure in the pipe at $L = 2000 \text{ m}$? Assume $\alpha = 1$.





Given:

$$D = 20 \text{ cm}, \dot{Q} = 0.06 \text{ m}^3/\text{s}, \alpha = 1, h_{\text{loss}} = \frac{0.02(L/D)V^2}{2g}$$

Find: pressure at $L = 2000 \text{ m}$?

Applying the energy equation between point 1 & 2

$$\left(h_p + \frac{p_1}{\rho g} + z_1 + \alpha_1 \frac{\bar{V}_1^2}{2g} \right)_{\text{Mech. part}} = \left(h_T + \frac{p_2}{\rho g} + gz_2 + \alpha_2 \frac{\bar{V}_2^2}{2g} \right)_{\text{Mech. part}} + h_{\text{Loss}}$$

$$V_1 = 0, \quad p_1 = 0, \quad z_1 = 100 \text{ m}, \quad z_2 = 20 \text{ m}, \quad V_2 = \frac{\dot{Q}}{A} = \frac{0.06}{\pi(0.02^2/4)} = 1.91 \text{ m/s}, \quad \alpha_1 = \alpha_2 = 1$$

$$h_p = 0, \quad h_T = 0, \quad D = 20 \text{ cm}$$

$$h_{loss} = \frac{0.02(L/D)V^2}{2g} = \frac{0.02(2000/0.2^2)1.19^2}{2 \times 9.81} = 37.2m$$

Substituting the values in the energy Eqn., the value of p_2 is found

$$\frac{p_2}{\gamma} = 100 - 20 - 0.186 - 0.0186L = 79.8 - 0.0186L$$

At $L = 2000$ m

$$\frac{p_2}{\gamma} = 79.8 - 37.2 = 42.6 \text{ m}$$

$$p_2 = 417.9 \text{ kPa}$$

END OF LECTURE (3)